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# EFFECT OF EQUAL CHANNEL ANGULAR PRESSING ON THE MECHANICAL PROPERTIES OF AL 4032–SiO<sub>2</sub> NANO COMPOSITE MATERIAL

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Abstract— The objective of the present study is to analyze the effect of Equal Channel Angular Pressing (ECAP) on the mechanical properties of Al4032–SiO<sub>2</sub> composite. These composites have been prepared by stir casting route in which the weight % SiO<sub>2</sub> nano particles are 0.25, 0.5, 0.75 and 1wt%. The ECAP process is done at a room temperature using a die with channel angle of 105° and corner angle 30°. The influence of ECAP on mechanical properties of Al4032 –SiO<sub>2</sub> composite is evaluated. In general in any composite the distribution of reinforcement particles can be observed with the micro-structural examination, but the effect of ECAP will be there on the mechanical properties of composite, so that here we have taken the evolution of Al4032-SiO<sub>2</sub> mechanical properties before and after ECAP process. As the agenda of ECAP is to improve the mechanical properties we have observed the great improvement in the mechanical properties.

Keywords—AL 4032, SiO2, Composite Material, Stir-Casting, ECAP, & Mechanical Properties.

#### I. INTRODUCTION

From the past few years, many of the researchers are focused on finding the light weight and better performance materials to replace the existing heavy weight materials [14,15]. The aluminium alloys (Al4032) are widely used for manufacturing the internal combustion pistons in place of cast iron and other heavy weight materials [1,3], because of their lesser weight[14,15]. Some of the researchers prepared the Al base metal matrix composites reinforced with  $SiO_2$  to enhance the mechanical properties [2,14,15]. To prepare the composite material people choose a best and easy process called stir casting process [4,5]. This process is widely used to prepare the composite materials.

But the major problem is dislocations or porosity or defects those occur in the composite material while casting. These defects reduce the strength of the materials. To overcome this issue we have advanced technique called sever plastic deformation. By using the SPD (sever plastic deformation) technique we can produce an ultrafine grained (UFG) and even Nano grained materials [7,8]. We have some of the SPD techniques to produce the UFG or Nano grained materials. These are 1. Equal Channel Angular Pressing (ECAP), 2. Multi Axial Compression (MAC), 3.High Pressure Torsion (HPT) and 4. Accumulative Roll Bonding (ARB) [7, 8],.5. Twist Extrusion (TE). In the above five methods the ECAP is most efficient and easiest technique [9, 10, 11].

. In the ECAP die we have two intersecting angles i.e. channel angle  $105^{\circ}$  ( $\Theta$ ) corner angle  $30^{\circ}$  ( $\Phi$ ). The sample specimen is simply pressed through the die with application of load and lubricant.



Figure-1: Equal Channel Angular Pressing Die

#### II. PREPARATION OF COMPOSITE MATERIAL

In this experiment we analysed the mechanical properties of Al4032 reinforced with  $SiO_2$  0.25, 0.5, 0.75 and 1 Wt%. By using stir casting we produced 16mm diameter and 200mm length rods by pouring molten metal into the permanent mould. The melting is done by open hearth furnace with a prepared mechanical stirrer. Once the material comes to liquid state the stirrer starts rotating with 250rpm by 20 minutes and then the reinforcement is added to molten Al4032 alloy. And then reinforced  $SiO_2$  is completely mixed with molten aluminium



Figure-2: Stir Casting Setup and Casting Mould

#### III. EXPERIMENTAL PROCEDURE:

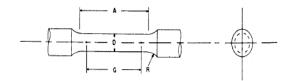
In this stage, the samples are machined into 14.6 mm diameter and 100 mm length rods from cast composite billets. For ECAP process, the surfaces of the samples are polished using emery paper to reduce the friction between die walls and surface of the samples [13]. The samples were subjected to ECAP using a die with two channels having an equal circular cross section with diameter of 15 mm. The two channels of the die intersect at angle of  $ext{0}$  and

 $\phi = 30^{\circ}$ . In order to reduce the drag friction between the die wall and sample surface lubricant is used [13].

#### IV. SPECIMEN PREPARATION:

The caste rods are machined into 14.6mm diameter and 100 mm length rods for ECAP process. After ECAP process the specimens are machined for mechanical tests like tensile test, compression test, Impact (IZOD-V) test, Impact (CHRPY-V) test and hardness tests. For specimen preparation we followed ASTM Standard dimensions.

**i. Tensile test**: The specimens are prepared as per ASTM E8/E8M-08 standards and in this the specimen dimensions are taken from the table of round tension test specimen and examples of small-size specimens Proportional to the standard specimen sub size 3 in for test specimens with gage length four times the diameter [e 8]



G—Gage length : 25 mm

D—Diameter : 6 mm

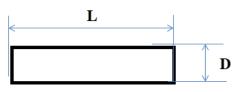
R—Radius of fillet : 6 mm

A—Length of reduced section : 30 mm



Figure-3: Tensile Test Specimen

ii. Compression Test: As per ASTM E 9 – 89a Suggested Solid Cylindrical Specimens.



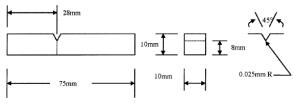
Diameter (D) :  $13 \pm 0.2$  mm Length (L) :  $39 \pm 1$ mm

L/D ratio : 3



Figure-4: Compression Test Specimen

iii. Impact (Izod-V) Test: As per ASTM E23 – 07a Izod (Cantilever-Beam) Impact Test Specimen, Type D.



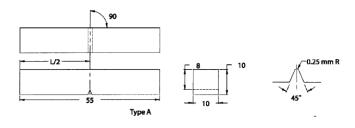
Length: 75 mm

Width : 10 mmHeight : 10 mmNotch depth : 2 mmNotch angle :  $45^{\circ}$ 



Figure-5: Izod Test Specimen

iv. Impact(chapry-V) Test: As per ASTM E23 – 07a Charpy (Simple-Beam) Impact Test Specimens, Type A



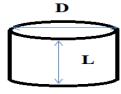
Length: 55 mm

 $\begin{tabular}{lll} Width & : 10mm \\ Height & : 10mm \\ Notch depth & : 2mm \\ Notch angle & : 45^\circ \\ \end{tabular}$ 



Figure-6: Charpy Test Specimen

### v. Hardness (Brinell) Test:



Diameter (D): 15 mm Length (L): 10 mm



Figure-7: Hardness Test Specimen

### V. ANALYSIS AND RESULTS:

To evaluate the mechanical properties like ultimate tensile strength, ultimate compressive load, impact strength and hardness test we performed some mechanical tests. These are, Tensile Test, Compression Test, Impact (IZOD-V) Test, Impact (CHRPY-V) Test and Hardness (Brinell) Tests.

### i. Tensile behavior of AL 4032-SiO<sub>2</sub> (02.5, 0.5, 0.75 and 1 Wt %).

The tensile behavior of AL  $4032\text{-SiO}_2(02.5, 0.5, 0.75 \text{ and } 1 \text{ Wt \%.})$  is evaluated as cast and after ECAP. The ultimate tensile strength of Al 4032- reinforced with  $0.5 \text{ Wt\% SiO}_2$  after ECAP is much higher than the before ECAP. Similarly the ultimate breaking load is greater for AL 4032- reinforced with  $0.25 \text{ Wt\% SiO}_2$  after ECAP sample among the all samples.

Table-1: Ultimate Load

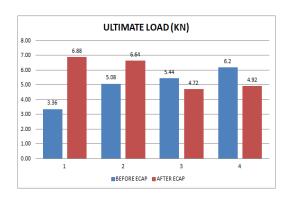


Chart-1: Ultimate Load (KN)

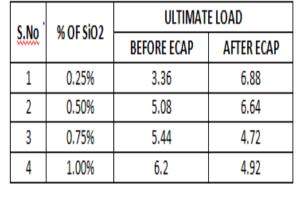


Table-2: Ultimate Tensile Strength (N/mm<sup>2</sup>)

50 -	ULTIMATE TENSILE STRENGTH (N/mm2														
50 -		215.877			- 2	222.074								Π	
00 -												198.9			
00								170.16	i						
50 -				152.14	1				1	34.66	5		14	9.635	í
									Ī		-				
00 -	97.902								Ц				ш		
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0 -															_
		1			2				3				4		
		1		■B	-	RE ECAI	P <b>=</b> A	AFTER E					4		

Chart-2: Ultimate Tensile Strength (N/mm<sup>2</sup>)

C No	% OF SiO2	ULTIMATE TENSILE STRENGTH					
S.No	70 UF 31UZ	BEFORE ECAP	AFTER ECAP				
1	0.25%	97.902	215.877				
2	0.50%	152.141	222 074				
3	0.75%	170.16	134.665				
4	1.00%	198.9	149.635				

**ELONGATION** S.No % OF SiO2 BEFORE ECAP AFTER ECAP 1 0.25% 0.76 1.28 2 2.96 0.50% 0.8 3 0.75% 2.16 0.32 4 1.00% 1.92 1.04

Table-3: Elongation (%)

ELONGATION (%)

3.5

3.5

2.96

2.16

2.16

1.92

1.04

0.5

0.32

0.32

0.32

0.32

0.32

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0.32

Chart-3: Elongation (%)

YIELD LOAD (KN)

7

6

5.96

6.16

5

4.72

4.32

4.32

1

0

1

2

3

4.72

4.32

4.32

4.32

4.32

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Chart-4: Yield Load (KN)

Table-4: Yield Lord (KN)

C No	% OF SiO2	YIELD LOAD					
S.No	70 0	BEFORE ECAP	AFTER ECAP				
1	0.25%	2.76	5.96				
2	0.50%	4.16	6.16				
3	0.75%	5.36	4.72				
4	1.00%	3.28	4.32				

Table-5: Yield Stress (N/mm<sup>2</sup>)

250 -		111	ELD STRES	) (IV)	/ 111111	12)			
				206.02					
200 -		187.01			Η,	167.657			
150 -							134.665		
.50			124.588				134.003		131.387
100 -								105.229	
100 -	80.42								
50 -									
0 -			2				3	4	4
	1	l		ORE ECA	Ρ 🕳 Δ	FTER ECA		4	4

Chart-5: Yield Stress (N/mm<sup>2</sup>)

C No	% OF SiO2	YIELD STRESS					
S.No	70 UF 31UZ	BEFORE ECAP	AFTER ECAP				
1	0.25%	80.42	187.01				
2	0.50%	124.588	206.02				
3	0.75%	167.657	134.665				
4	1.00%	105.229	131.387				

### ii. Compressive behavior of AL 4032-SiO<sub>2</sub> (0.25, 0.5, 0.75 and 1 Wt %).

The compressive behavior of AL  $4032\text{-SiO}_2$  (0.25, 0.5, 0.75 and 1 Wt %.) were evaluated as cast and after ECAP process samples. The ultimate compressive load is maximum for AL 4032- reinforced with 0.5 Wt% SiO<sub>2</sub> before ECAP sample.

ULTIMATE COMPRESSION LOAD (KN)

50

50

41.68

42.64

44.68

32.88

33.92

34.56

37.4

37.4

38.88

39.92

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Chart-6: Ultimate Compression Load (KN)

Table-6: Ultimate Compression Load (KN)

C No	% OF SiO2	ULTIMATE COMPRESSION LOAD				
S.No	70 01 3102	BEFORE ECAP	AFTER ECAP			
1	0.25%	41.68	32.88			
2	0.50%	50.88	35.92			
3	0.75%	47.64	34.56			
4	1.00%	44.68	37.4			

### iii. Impact strength of AL 4032-SiO<sub>2</sub> (0.25, 0.5, 0.75 and 1 Wt %).

The impact strength of AL 4032-SiO<sub>2</sub> (0.25, 0.5, 0.75 and 1 Wt %.) were evaluated as cast and after ECAP process samples for both IZOD and CARPY tests .In both the cases the breaking load of Al4032-reinforced with 0.25, 0.5, 0.75 and 1 Wt % of SiO<sub>2</sub> after ECAP samples are having maximum values.

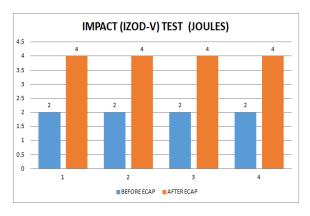


Chart-7: Impact (Izod-V) Test (Joules)

	N 050'00	IMPACT (IZOD-V) TEST IN JOULES					
S.No	% OF SiO2	BEFORE ECAP	AFTER ECAP				
1	0.25%	2	4				
2	0.50%	2	4				
3	0.75%	2	4				
4	1.00%	2	4				

Table-7: Impact (Izod-V) Test (Joules)

Table-8: Impact (Charpy-V) Test (Joules)

			IMI	PACT (	CHRP	Y) T	EST (.	IOULI	ES)			
_												
					6							6
_												
		4						4				
-			$\vdash$						-		-	
	2			2			2			2		
_												
_			_					_			Н	
_		1		2				3			4	
					FORE ECA	\D =	AFTER EC					

Chart-8: Impact (Charpy-V) Test (Joules)

c	No	% OF SiO2	IMPACT (CHARPY) TEST IN JOULES					
3,	.No	70 UF 31UZ	BEFORE ECAP	AFTER ECAP				
	1	0.25%	2	4				
	2	0.50%	2	6				
	3	0.75%	2	4				
	4	1.00%	2	6				

### iv. Hardness (Brinell) test of AL 4032-SiO<sub>2</sub> (0.25, 0.5, 0.75 and 1 Wt %).

The hardness of the AL  $4032\text{-SiO}_2$  (0.25, 0.5, 0.75 and 1 Wt %.) were evaluated as cast and after ECAP. The Brinell hardness number (HB) is maximum for AL 4032- reinforced with 0.25 Wt% SiO<sub>2</sub> after ECAP.

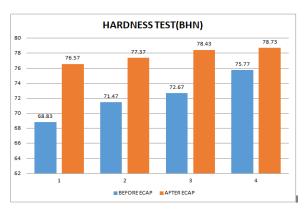


Chart-7: Hardness Results (BHN)

C No	% OF SiO2	HARD NESS TEST(BHN)					
S.No	70 UF 3IUZ	BEFORE ECAP	AFTER ECAP				
1	0.25%	68.83	76.57				
2	0.50%	71.47	77.37				
3	0.75%	72.67	78.43				
4	1.00%	75.77	78.73				

Table-8: Hardness Results (BHN)

#### VI. CONCLUSIONS:

In the present investigation the following conclusions are drawn.

- 1. The stir casting method was successfully employed for casting of Al4032 composite reinforced with sio2. The experimental study reveals that the distributions of particulates in the matrix are uniform.
- 2. The effect of the SiO<sub>2</sub> reinforcement on AL 4032 metal matrix is appreciable in Ultimate tensile strength, Impact and hardness after ECAP.
- 3. After ECAP process, the size and distribution of the SiO<sub>2</sub> partials are not changed but significant reduction in the grain size of matrix alloy was observed based on the mechanical tests.
- 4. By increasing the %SiO<sub>2</sub> the impact strength is increased.
- 5. The maximum value of ultimate tensile strength through the ECAP process is exhibited by AL 4032-reinforced with 1Wt% SiO<sub>2</sub>.
- 6. Also the maximum hardness exhibited by AL 4032- reinforced with 1Wt% SiO<sub>2</sub>. After ECAP.
- 7. Hence I conclude that the mechanical properties of AL 4032- reinforced with 1Wt% SiO<sub>2</sub> are dramatically increased after ECAP except in compression strength.

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